

# Implementation of RGA and Decoupler for the Fluid Catalytic Cracking Unit in Petroleum Refinery

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*Abstract*— This paper gives the numerical model, the utilization of RGA examination and decoupler to the Fluid Catalytic Cracking Unit (FCCU). A mind boggling dynamic model of the reactor–regenerator framework is created and therefore utilized in the regulator. An average FCC unit measures a lot of the feedstock into more significant items. The general monetary advantages of a refining could be significantly expanded if appropriate control and streamlining techniques are executed. Control of the FCC keeps on being a difficult and significant issue. A control framework is made out of a few collaborating control circles. The quantity of plausible elective setups of control circles is exceptionally huge. Multi circle control frameworks are frequently utilized for multivariable cycles due to their straightforwardness. Relative addition exhibit is utilized to limit the communication and select the variable pairings and afterward decoupler is created to eliminate connection totally.

*Index Terms*— FCCU, Control, RGA, Decoupler

## 1. Introduction

For more than 60 years, reactant breaking has been one of the fundamental cycles in oil refining, having gone through fabulous turn of events. The liquid reactant breaking unit (fccu) has become the "test seat" of many progressed control strategies. Today, both scholarly world and industry are communicating incredible interest in the improvement of new control calculations and in their proficient modern fcc execution. Investigation and control of fcc measure have been known as trying issues because of the accompanying cycle qualities, ( i ) convoluted and mostly secret hydrodynamics, ( ii ) complex energy of both breaking and coke consuming responses, (iii) solid association between the reactor and regenerator, (iv) many working imperatives. Fccu's consistent state conduct is profoundly nonlinear, prompting various consistent states, input multiplicities and so on in prior years before the improvement of zeolite impetuses, the significant control issue was one of adjustment, of simply keeping the unit running. Later with zeolite impetuses, the accentuation is moved to expanding creation rates notwithstanding unit limitations and to deal with heavier feeds. The necessities for reformulated gas have added the need to control item arrangement. This is more perplexing issue since the quantity of cycle factors that one might want to control considerably surpasses the quantity of controlled factors that are accessible for the undertaking.

## 2. FCCU unit

Fluidized synergist breaking in FCC unit is a significant cycle in petroleum processing plants. It overhauls weighty hydrocarbons to lighter more important items by breaking, and is the significant maker of fuel in treatment facilities. FCCU's present testing multivariable control issues. The model comprises of subsystems: take care of and preheat framework, reactor, regenerator, air blower, wet gas blower and impetus course lines. The reactor and regenerator are more significant for the FCCU cycle. It comprises of various complex compound/actual cycles. Model: synergist breaking compound responses, three stage (gas-fluid strong) liquid elements, insecure state heat move, and so on In this cycle the synergist movement, multiphase mass fluidized status and other working boundaries (for example response temperature and framework pressure and so forth are basic for balancing out the activity and creating the certified oil items with high productivity.

### A. Process Description

The schematic stream outline of an average current FCC unit appeared in Fig. the following depends on the "next to each other" setup. The preheated high bubbling oil feedstock (at around 315 to 430 °C) comprising of long chain hydrocarbon particles is joined with reuse slurry oil from the lower part of the refining section

and infused into the impetus riser where it is disintegrated and broken into more modest atoms of fume by contact and blending in with the extremely hot powdered impetus from the regenerator. The entirety of the breaking responses occur in the impetus riser. The hydrocarbon fumes "fluidize" the powdered impetus and the combination of hydrocarbon fumes and impetus streams upward to enter the reactor at a temperature of around 535 °C . The reactor is truth be told simply a vessel in which the broke item fumes are: (a) isolated from the alleged spent impetus by coursing through a bunch of two-stage inside the reactor (b) the spent impetus streams descending through a steam stripping segment to eliminate any hydrocarbon fumes before the spent impetus re-visitations of the impetus regenerator. The progression of spent impetus to the regenerator is directed by a slide valve in the spent impetus line. Since the breaking responses produce some carbonaceous material (alluded to as coke) that stores on the impetus and rapidly lessens the impetus reactivity, the impetus is recovered by consuming off the saved coke with air blown into the regenerator. The regenerator works at a temperature of around 715 °C. The burning of the coke is and it delivers a lot of warmth that is mostly consumed by the recovered impetus and gives the warmth needed to the vaporization of the feedstock and the endothermic breaking responses that occur in the impetus riser. Hence, FCC units are frequently alluded to as being heat adjusted.

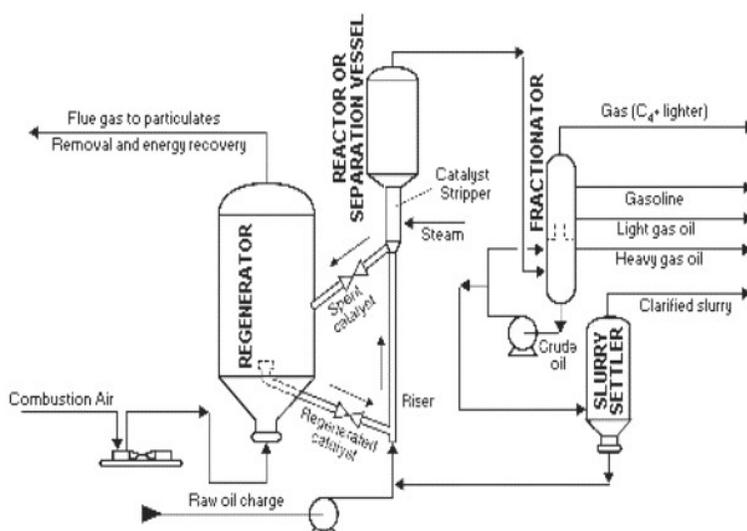


Figure1.Schematic representation of FCC unit

The hot impetus (at around 715 °C) leaving the regenerator streams into an impetus withdrawal well where any entrained burning pipe gas are permitted to get away and stream once again into the upper part to the regenerator. The progression of recovered impetus to the feedstock infusion point underneath the impetus riser is managed by a slide valve in the recovered impetus line. In this cycle the significant estimated factors are picked to be the reactor temperature/riser outlet temperature ( $T_{RA}$ ) and the regenerator gas temperature ( $T_{RG}$ ). The controlled factors are stream pace of recovered impetus ( $R_{RC}$ ), stream pace of spent impetus ( $R_{SC}$ ) and stream pace of air to the regenerator ( $R_{AI}$ ).

### 3.Model for FCCU

The demonstrating of complex substance frameworks for the reproduction of cycle elements and control has been spurred by the monetary motivators for development of plant activity and plant plan, as on account of FCCU. The vast majority of the monetary increase from FCC control improvement has originated from the enhancement level, with the guideline framework basically giving steady, responsive, and safe activity. The issue is to discover controller conspires that are (1) Effective, (2) Economically supported, (3) Related to existing practice, and (4) Able to give satisfactory administrator interface when wanted.

### A. Development of Model

A static model is utilized for the riser. In this work, a powerful down to earth control plan of Joseph A. Bromley and Thomas J. Ward (1981) is utilized. In this plan, feed is gasoil which can break into fuel or light gas. The equilibrium condition for Hold up of impetus:

$$\frac{dH_{RA}}{dt} = [R_{RC} - R_{SC}]$$

Note:

$$\frac{dH_{RG}}{dt} = -\frac{dH_{RA}}{dt}$$

### B. Reactor Model

The impetus is steam-stripped in the reactor vessel to eliminate hydrocarbons. The reactor overhead is isolated in a twister to eliminate impetus and the item fumes pass to an item fractionator. The equilibrium condition of reactor temperature is given by,

$$\frac{dT_{RA}}{dt} = \frac{R_{RC}}{H_{RA}}(T_{RG} - T_{RA}) + \frac{1}{S_C H_{RA}} [-S_F D_{TF} R_{TF}(T_{RA} - T_{TF}) - \Delta H_{FV} D_{TF} R_{TF}] - \frac{\Delta H_{CR} R_{OC}}{S_C H_{RA}}$$

$$R_{OC} = D_{TF} R_{TF} C_{TF}$$

$$\frac{C_{TF}}{1 - C_{TF}} = \frac{K_{CR} P_{RA} H_{RA}}{R_{TF}}$$

### C. Regenerator Model

The balance equation of Regenerator temperature is given by,

$$\frac{dT_{RG}}{dt} = \frac{R_{SC}}{H_{RG}}(T_{RA} - T_{RG}) + \frac{1}{S_C H_{RG}} [-S_A R_{AI}(T_{RG} - T_{AI}) + \Delta H_{RG} R_{CB}]$$

$$R_{CB} = \left(\frac{R_{AI}}{C_1}\right) (21 - O_{FG})/100$$

## 4. Control of FCCU

The control of introduced factors is significant for the proficient and safe activity of the unit and has direct effect on the items yield. Control of the FCC has been and persistent testing and significant issue. As will be seen, its consistent state conduct is exceptionally non straight, prompting various consistent states, input multiplicities, and all that infers.

The reactor temperature must be kept up at a specific level to give an ideal greatest transformation of the feed oil. A legitimate reactor temperature control implies additionally a decent administration of warm energy. Control of reactor impetus stock is important to give adjustment and wellbeing in the impetus flow. Reactor pressure control legitimately impacts the coke and gases development. Piece of the items must be kept up at wanted certain qualities to guarantee the items quality and plant efficiency. The stream moves the response items overhead to the items recuperation segment. The standpipe moves spent impetus persistently from the separator to the regenerator by a control valve. In the regenerator, spent impetus particles are scorched within the sight of air. The wind current rate to the regenerator is constrained by a control valve that vents segments of the air to the air. On the highest point of the regenerator, tornadoes play out the impetus partition from the vent gas stream.

### A. Interaction of Control Loops

Consider a process with two controlled outputs and two manipulated inputs in figure 2.

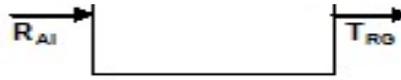


Figure 2. MIMO system

The input-output relationships are given by

$$y_1(s) = G_{11}(s)m_1(s) + G_{12}(s)m_2(s) \quad (4.1)$$

$$y_2(s) = G_{21}(s)m_1(s) + G_{22}(s)m_2(s) \quad (4.2)$$

Where  $G_{11}(s)$ ,  $G_{12}(s)$ ,  $G_{21}(s)$  and  $G_{22}(s)$  are the four transfer functions relating the two inputs and the two outputs. These equations indicate that the change in  $m_1$  or  $m_2$ , will affect both controlled outputs. Two potential problems arise from this process interaction:

- It may destabilize the shut circle framework
- It will in general make regulator tuning more troublesome.

### B. Relative Gain Array

Relative addition exhibit gives a proportion of cooperation dependent on consistent state conditions. It is utilized to choose the sets of information and yield factors so as to limit the measure of association among the subsequent circles. Relative addition exhibit is communicated as Relative increase cluster is communicated as

$$\lambda = \begin{bmatrix} \lambda_{11} & \lambda_{12} \\ \lambda_{21} & \lambda_{22} \end{bmatrix}$$

In particular

- i) If  $\lambda_{11} = 0$ , then  $y_1(T_{RA})$  does not act in response to  $m_1(R_{RC})$  and  $m_1$  should not be worn to control  $y_1$ .
- ii) If  $\lambda_{11} = 1$ , then  $m_2(R_{AI})$  does not impinge on  $y_1$  and the control loop between  $y_1$  and  $m_1$  does not interrelate with loop of  $y_2(T_{RG})$  and  $m_2$ .
- iii) If  $0 < \lambda_{11} < 1$ , then the dealings exists and as  $m_2$  varies it affects the stable condition value of  $y_1$  the smaller value of  $\lambda_{11}$ , the larger interaction becomes.
- iv) If  $\lambda_{11} < 0$ , then  $m_2$  causes strong effects on  $y_1$  and in opposite direction from that caused by  $m_1$ .

The imperative feedback that provide automatic control of FCCU are, (i) Control of reactor temperature( $T_{RA}$ ) by manipulation of the regenerated catalyst rate( $R_{RC}$ ) and (ii) Control of regenerator temperature( $T_{RG}$ ) by manipulation of the air flow rate( $R_{AI}$ ).

### C. Design of Non Interacting Control Loops

The general increase cluster shows how the sources of info ought to be combined with the yields to shape circles with the more modest measure of cooperation. To drop the cooperation impacts between two circles, a Decoupler is utilized.

### D. Decoupling Control System

Fundamental Idea is to utilize extra regulators to make up for measure connection and accordingly lessen control circle collaboration. In a perfect world; decoupling control permits set guide changes toward influence just the ideal controlled factors. Regularly, decoupling regulators are planned utilizing a basic cycle model (for example consistent state model or move work model). Two control loops by coupling  $m_1$  with  $y_1$  and  $m_2$

with  $y_2$  is formed .From fig [2], to keep  $y_1$  constant,  $m_1$  should be changed by the following amount:

$$m_1 = -\frac{G_{12}(s)}{G_{11}(s)}m_2 \tag{4.3}$$

Above equation implies a dynamic element with transfer function

$$D_1(s) = -\frac{G_{12}(s)}{G_{11}(s)} \tag{4.4}$$

This dynamic component is known as a Decoupler. It drops any impact that circle 2 may have on circle 1. To dispense with the cooperation from circle 1 to circle 2, use the dynamic element  $D_2(s)$ .

$$D_2(s) = -\frac{G_{21}(s)}{G_{22}(s)} \tag{4.5}$$

### 5.RESULTS AND DISCUSSION

The research on the dynamic characteristics of FCC unit reveals that FCC processes consist of two input and two outputs. For practical combustion mode, a common choice of variables to be regulated is the riser outlet temperature ( $T_{RA}$ ) and the temperature of regenerator's temperature ( $T_{RG}$ ). If the pairings  $T_{RA} - R_{RC}$  and  $T_{RG} - R_{RI}$  are selected to design a decentralized control strategy ,a classical rise-regenerator control structure is obtained . The mathematical model considered in this work simulates the main features of the behavior of FCC units ,as it is shown in figure 3 and figure 4.

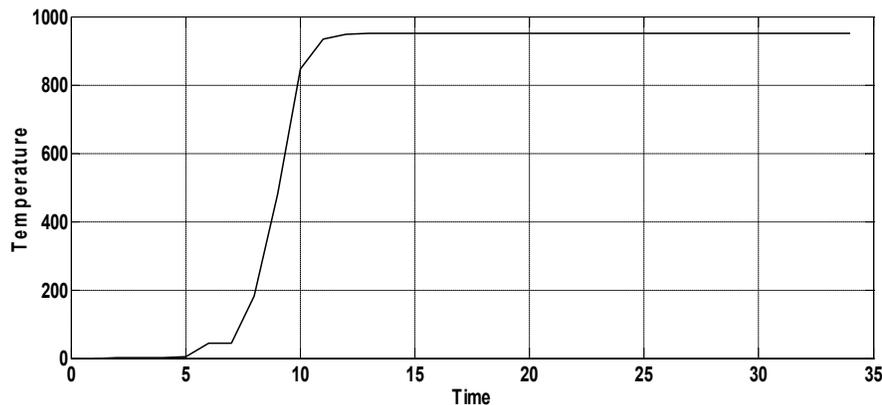


Figure 3.Steadystate Response of  $T_{RA}$

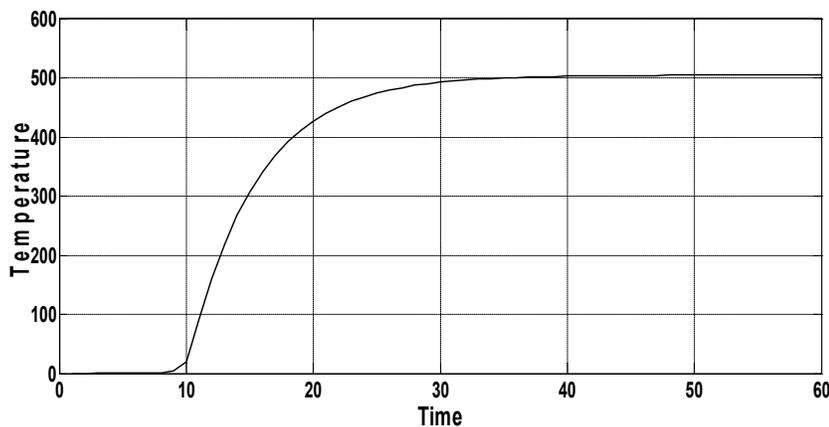


Figure 4. Steadystate Response of  $T_{RG}$

A. Relative Gain Array Analysis

For the choice of pairing the response obtained is shown in figure (5) and (6).

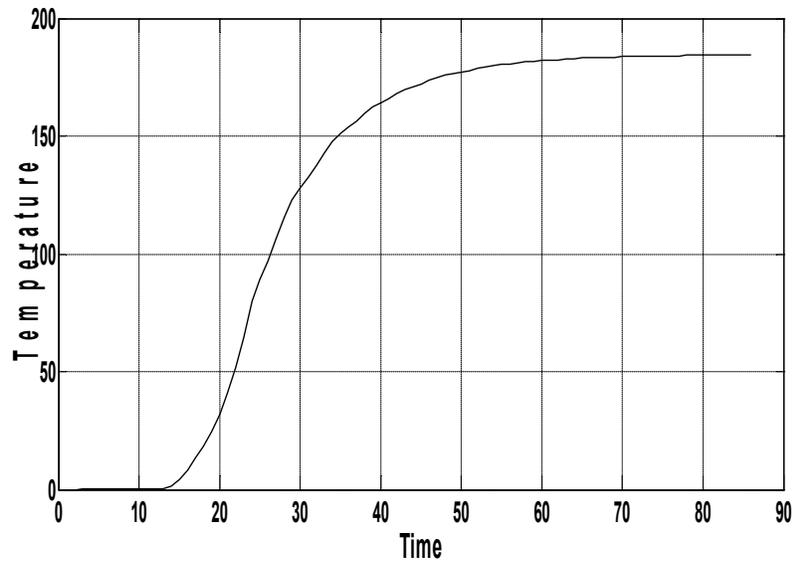


Figure 5. Regenerator Temperature response while  $m_1$  constant

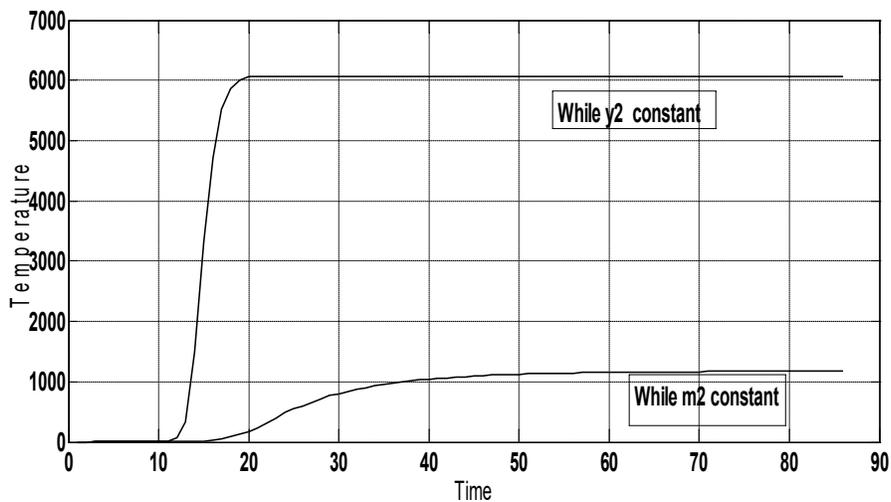


Figure 6. Reactor Temperature responses while  $m_1$  &  $y_1$  constant

For this choice of pairing the relative gain matrix obtained is

$$\lambda = \begin{bmatrix} 0.98 & 0.02 \\ 0.02 & 0.98 \end{bmatrix}$$

So the desirable pairing is to couple  $m_1$  with  $y_1$  and couple  $m_2$  with  $y_2$ .

### B. Decoupler Design

Since there is some interaction between two loops, decoupler is used to cancel the interaction. The dynamic elements of decouplers are designed using the formula's given in [4.4] & [4.5]. The simulation result using decoupler is shown in figure 7.

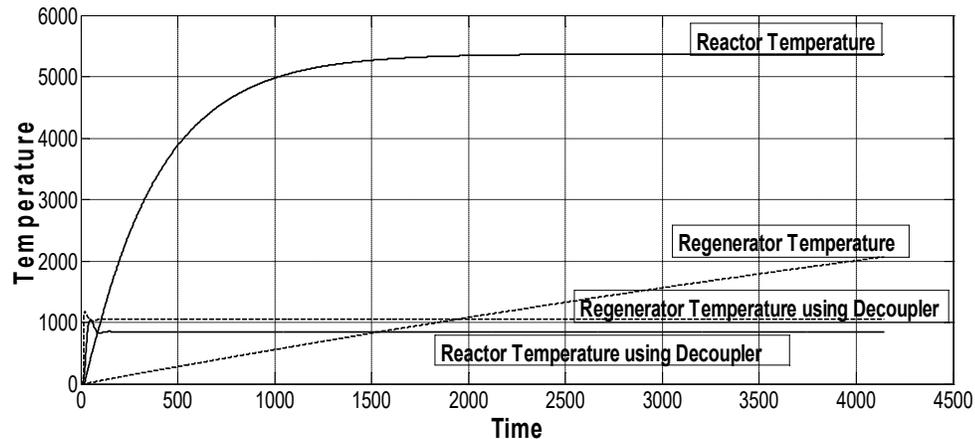


Figure 7. Comparison graph for  $T_{RR}$  and  $T_{RG}$  using decoupler

## 6. CONCLUSION

The demonstrating of fluidized synergist breaking is introduced here. For this communication cycle, determination of blending is finished by relative increase exhibit. As per RGA grid, the factors are matched and again circle reaction is found. Prescribed matching to limit the association is found by RGA investigation. To eliminate the operation totally, decouplers are planned and actualized utilizing MATLAB.

## 7. FUTURE WORK

The state space model of FCCU has to be extended for dynamic model and the Model Predictive Control scheme has to be implemented for the same. To analyze the effect of reactor temperature and regenerator temperature in conversion of total feed (volume fraction) using MPC.

### Nomenclature

- $C_1$  - Fitting constant for particular data
- $C_{CAT}$  - Concentration of catalytic carbon on catalyst, wt%
- $C_{RC}$  - Concentration of regenerated catalyst, wt%
- $C_{SC}$  - Concentration of spent catalyst, wt%
- $C_{TF}$  - Conversion of total feed, volume fraction
- $D_{TF}$  - Density of total feed,  $kg/m^3$
- $F_{CF}$  - Factor for carbon formation of feed,  $(kg\ carbon/s) / (m^3/s)$
- $H_{RA}$  - Hold up of catalyst in the reactor, Kg
- $H_{RG}$  - Hold up of catalyst in the regenerator, Kg
- $O_{FG}$  - Oxygen in flue gas, mol%
- $R_{AI}$  - Rate of regenerator air, kg/s
- $R_{CB}$  - Rate of coke burning, kg/s
- $R_{CC}$  - Rate of catalytic carbon formation in the reactor, kg/s
- $R_{CF}$  - Rate of carbon forming on catalyst, kg/s
- $R_{OC}$  - Rate of gas oil cracking, kg/s

$R_{RC}$  - Rate of regenerated catalyst, Kg/s  
 $R_{SC}$  - Rate of spent catalyst, kg/s  
 $R_{TF}$  - Rate of total feed,  $m^3/s$   
 $S_A$  - Specific heat of air, J/kg-k  
 $S_C$  - Specific heat of catalyst, J/kg-k  
 $T_{AI}$  - Temperature of air, K  
 $T_{RA}$  - Temperature of Reactor, K  
 $T_{RG}$  - Temperature of Regenerator, K  
 $T_{TF}$  - Temperature of feed, K  
 $\Delta H_{CR}$  - Heat of cracking, J/kg  
 $\Delta H_{FV}$  - Heat of feed vaporization, J/kg  
 $\Delta H_{RG}$  - Heat of regeneration (coke burning), J/kg

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